











SLVS530D - SEPTEMBER 2005 - REVISED OCTOBER 2015

TPS63700

TPS63700 DC-DC Inverter

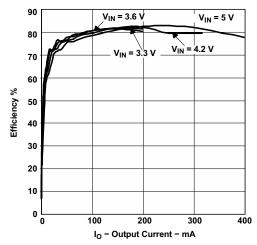
Features

- Adjustable Output Voltage Down to -15 V
- 2.7-V to 5.5-V Input Voltage Range
- Up to 360-mA Output Current
- 1000-mA Typical Switch Current Limit
- Up to 84% Efficiency
- Typical 1.4-MHz Fixed-Frequency PWM Operation
- Thermal Shutdown
- Typical –19-V Output Overvoltage Protection
- 1.5-µA Shutdown Current
- Small 3-mm × 3-mm SON-10 Package (DRC)

Applications

- Generic Negative Voltage Supply
- Small-to-Medium Size OLED Displays
- Bias Supply

Efficiency vs Output Current



3 Description

The TPS63700 is an inverting DC/DC converter generating a negative output voltage down to -15 V with output currents up to 360 mA, depending on input-voltage to output-voltage ratio. With a peak efficiency of 84%, the device is ideal for portable battery-powered equipment. The input voltage range of 2.7 V to 5.5 V allows the TPS63700 to be directly powered from a Li-ion battery, from 3-cell NiMH/NiCd, from a 3.3-V or 5-V supply rail.

The inverter operates with a fixed-frequency pulse width modulation (PWM) control topology. The device has an internal current limit, overvoltage protection, and a thermal shutdown for highest reliability under fault conditions.

A switching frequency of typically 1.4 MHz allows the use of small external components enabling a small solution size.

The TPS63700 comes in a small 3-mm x 3-mm SON-10 package.

Device Information⁽¹⁾

PART NUMBER	PACKAGE	BODY SIZE (NOM)
TPS63700	VSON (10)	3.00 mm x 3.00 mm

(1) For all available packages, see the orderable addendum at the end of the datasheet.

Typical Application Schematic

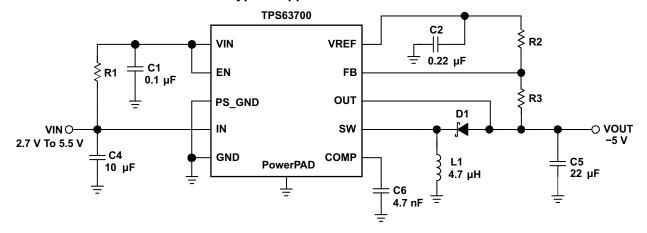




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4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

Changes from Revision C (June 2013) to Revision D

Page

Changes from Revision B (November 2007) to Revision C

Page

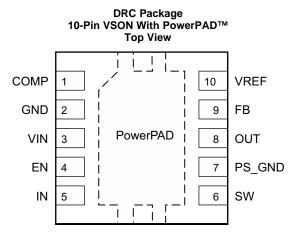
Deleted Dissipation Ratings table and added Thermal Information table.

4

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5 Pin Configuration and Functions



Pin Functions

PIN		I/O	DESCRIPTION
NAME	NO.	1/0	DESCRIPTION
COMP	1	I/O	Compensation pin for control, connect a 4.7 nF capacitor between this pin and GND
GND	2	_	Ground pin
VIN	3	1	Supply voltage input for control logic, connect a RC circuit of 10R and 100 nF to filter this supply voltage
EN	4	1	Enable pin (EN = GND: disabled; EN = VIN: enabled)
IN	5	ı	Supply voltage for the power switch
SW	6	0	Inverter switch output
PS_GND	7	ı	Connect to GND for control logic
OUT	8	1	Output voltage sense input
FB	9	I	Feedback pin for the voltage divider
VREF	10	0	Reference voltage output. Connect a 220-nF capacitor to ground. Connect the lower resistor of the negative output voltage divider to this pin.



6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range unless otherwise noted⁽¹⁾

	MIN	MAX	UNIT
Input voltage at VIN ⁽²⁾	-0.3	6	V
Input voltage at IN ⁽²⁾		VIN	V
Minimum voltage at OUT (2)		-18	V
Voltage at EN, FB, COMP, PS_GND (2)	-0.3	V _{IN} + 0.3	V
Differential voltage between OUT to VIN (2)		24	V
Operating virtual junction temperature, T _J	-40	150	°C
Storage temperature, T _{stg}	-65	150	°C

⁽¹⁾ Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) All voltage values are with respect to network ground terminal, unless otherwise noted.

6.2 ESD Ratings

			VALUE	UNIT
		Human body model (HBM), per ANSI/ESDA/JEDEC JS-001, all pins (1)	±2000	
V _(ESD)	Electrostatic discharge	Charged device model (CDM), per JEDEC specification JESD22-C101, all pins (2)	±1000	V

⁽¹⁾ JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

6.3 Recommended Operating Conditions

	MIN	MAX	UNIT
Input voltage range, V _{IN}	2.7	5.5	٧
Operating free-air temperature, T _A	-40	85	Ô
Operating virtual junction temperature, T _J	-40	125	٥°

6.4 Thermal Information

		TPS63700	
	THERMAL METRIC ⁽¹⁾	DRC (VSON)	UNIT
		10 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	41.2	°C/W
$R_{\theta JC(top)}$	Junction-to-case(top) thermal resistance	62.8	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	16.6	°C/W
ΨЈТ	Junction-to-top characterization parameter	1.2	°C/W
ΨЈВ	Junction-to-board characterization parameter	16.8	°C/W
R _{0JC(bot)}	Junction-to-case(bottom) thermal resistance	4.1	°C/W

 For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report, SPRA953.

⁽²⁾ JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.



6.5 Electrical Characteristics

-40°C to 85°C, over recommended input voltage range, typical at an ambient temperature of 25°C (unless otherwise noted)

	PARAMETER	(1)	TEST CONDITIONS	MIN	TYP	MAX	UNIT
SUPPLY	′						
V _{IN}	Input voltage range		Pin VIN, IN	2.7		5.5	V
I _(Q)	Quiescent	VIN	$V_{IN} = 3.6 \text{ V}, I_{OUT} = 0,$		330	400	μΑ
	current	IN	$EN = V_{IN}$, no switching $V_{OUT} = -5 V$		640	750	μΑ
I _{SD}	Shutdown supply current		EN = GND		0.2	1.5	μΑ
UVLO	Undervoltage lockout threshold			2.1	2.35	2.7	V
	Thermal shutdown temperatur	е			150		°C
T _{SD}	Thermal Shutdown hysteresis		Junction temperature decreasing		5		°C
CONTRO	OL STAGE						
V _{EN}	High level input voltage			1.4			V
V _{EN}	Low level input voltage					0.4	V
I _{EN}	Input current		$EN = V_{IN}$ or GND		0.01	0.1	μΑ
POWER	SWITCH					•	
I _{LIM}	Inverter switch current limit		$2.7 \text{ V} < \text{V}_{\text{IN}} < 5.5 \text{ V}$	860	1000	1140	mA
Б	la contan accidaba a a mariatana a		V _{IN} = 3.6 V		440	600	mΩ
R _{DS(ON)}	Inverter switch on-resistance		$V_{IN} = 5 V$		370	500	11122
D _{MAX}	Maximum duty cycle inverting converter				87.5%		
D _{MIN}	Minimum duty cycle inverting converter				12.5%		
f _S	Oscillator frequency			1250	1380	1500	kHz
ОИТРИТ	Г						
V _{OUT}	Adjustable output voltage range			-15		-2	V
V _{OUT}	DC output accuracy		PWM mode, device switching		±3%		
V _{REF}	Reference voltage		I _{REF} = 10 μA	1.2	1.213	1.225	V
V _{OVP}	Output overvoltage protection				-19		V
V _{FB}	Negative feedback regulation voltage		V _{IN} = 2.7 V to 5.5 V	-0.024	0	0.024	V
I _{FB}	Negative feedback input bias	current	$V_{FBN} = 0.1 V_{REF}$		2		nA

⁽¹⁾ Parameter does not include tolerance of external resistors.



6.6 Typical Characteristics

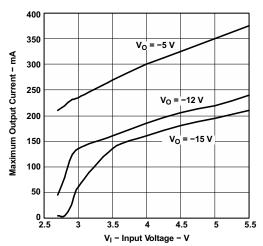


Figure 1. Maximum Output Current vs Input Voltage

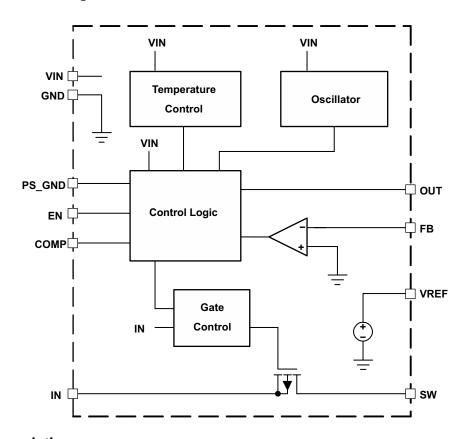


7 Detailed Description

7.1 Overview

The TPS63700 is a DC/DC converter for negative output voltages using buck-boost topology. It operates with an input voltage range of 2.7 V to 5.5 V and generates a negative output voltage down to −15 V. The output is controlled by a fixed-frequency, pulse-width-modulated (PWM) regulator. In normal operation mode, the converter operates at continuous conduction mode (CCM). At light loads it can enter discontinuous conduction mode (DCM).

7.2 Functional Block Diagram



7.3 Feature Description

7.3.1 Enable

Applying GND signal at the EN pin disables the converter, where all internal circuitry is turned off. The device now just consumes low shutdown current flowing into the VIN pin. The output load of the converter is also disconnected from the battery as described in *Load Disconnect*. Pulling the EN pin to V_{IN} enables the converter. Internal circuitry, necessary to operate the converter, is then turned on.

7.3.2 Load Disconnect

The device supports complete load disconnection when the converter is disabled. The converter turns off the internal PMOS switch, thus no DC current path remains between load and input voltage source.

7.3.3 Output Overvoltage Protection

The converter has an output overvoltage protection implemented. The output voltage is limited to -19 V in case the feedback connection from the output to the FB pin is open.



Feature Description (continued)

7.3.4 Undervoltage Lockout

An undervoltage lockout prevents the device from starting up and operating if the supply voltage at VIN is lower than the programmed threshold shown in the *Electrical Characteristics* table. The device automatically shuts down the converter when the supply voltage at VIN falls below this threshold. Nevertheless, parts of the control circuits remain active, which is different than device shutdown using EN inputs. The undervoltage lockout function is implemented to prevent device malfunction.

7.3.5 Overtemperature Shutdown

The device automatically shuts down if the implemented internal temperature detector detects a chip temperature above the programmed threshold shown in the electrical characteristics table. It starts operating again when the chip temperature decreases. A built-in temperature hysteresis avoids undefined operation caused by ringing from over-temperature shutdown.

7.4 Device Functional Modes

7.4.1 Soft-Start

The converter has a soft-start function. When the converter is enabled, the implemented switch current limit ramps up slowly to its nominal value. Soft-start is implemented to limit the input current during start-up to avoid high peak currents at the battery which could interfere with other systems connected to the same battery.

Without soft-start, uncontrolled input peak currents flow to charge up the output capacitors and to supply the load during start-up. This would cause significant voltage drops across the series resistance of the battery and its connections.

7.4.2 PWM Operation

The converter operates in a fixed-frequency, pulse-width-modulated control scheme. The on-time of the switches varies depending on input-to-output voltage ratio and the load. During this on-time, the inductor connected to the converter is charged with current. In the remaining time, the time period set by the fixed operating frequency, the inductor discharges into the output capacitor via the rectifier diode. At medium to heavy loads the inductor current is continuous and the device operates in continuous conduction mode (CCM).

7.4.3 Power Save Mode Operation

As the load current decreases, the converter enters Power Save Mode. Entering Power Save Mode happens at the boundary to discontinuous conduction mode (DCM). During light load, the inductor current of this converter can become discontinuous. In this case, the control circuit of the controller output automatically takes care of these changing conditions to always operate with an optimum control setup.

7.4.4 Control

The controller circuit of the converter is based on a fixed-frequency, multiple-feed-forward controller topology. Input voltage, output voltage, and voltage drop across the switch are monitored and forwarded to the regulator. Changes in the operating conditions of the converter directly affect the duty cycle.

The error amplifier compares the voltage at FB pin with GND to generate an accurate and stable output voltage. The error amplifier is internally compensated. At light loads, the converter operates in discontinuous conduction mode (DCM).

If the load will be further decreased, the energy transmitted to the output capacitor cannot be absorbed by the load and would lead to an increase of the output voltage. In this case, the converter limits the output voltage increase by skipping switch pulses.

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8 Application and Implementation

NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

8.1 Application Information

The TPS63700 DC/DC converter is intended for systems typically powered by a single-cell Li-ion or Li-polymer battery with a terminal voltage between 2.7 V up to 4.2 V. Due to the recommended input voltage going up to 5.5 V, the device is also suitable for 3-cell alkaline, NiCd,or NiMH batteries, as well as regulated supply voltages of 3.3 V or 5 V.

8.2 Typical Application

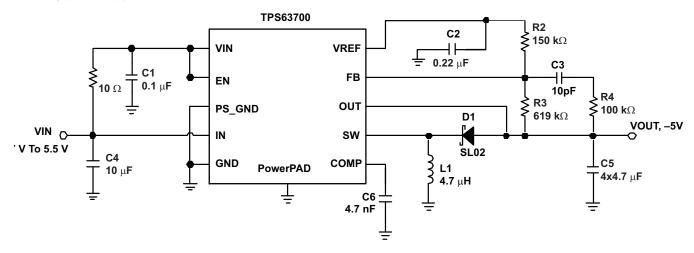


Figure 2. Circuit for -5-V Output

8.2.1 Design Requirements

The design of the inverter can be adapted to different output voltage and load current needs by choosing external components appropriately. The following design procedure is adequate for the whole V_{IN} , V_{OUT} and load current range of TPS63700.

Table 1 shows the list of components for the *Application Curves*.

Table 1. List of Components

REFERENCE	DESCRIPTION
C1, C2, C3, C4,	X7R/X5R ceramic
C5	4 x 4.7 μF X7R/X5R ceramic
D1	SL03/SL02 Vishay
L1	-5V: TDK VLF4012 4R7, TDK SLF6025-4R7, Coilcraft LPS4018-472,
	–12V: Sumida CDRH5D18 10 μH



8.2.2 Detailed Design Procedure

8.2.2.1 Programming the Output Voltage: Converter

The output voltage of the TPS63700 converter can be adjusted with an external resistor divider connected to the FB pin. The reference point of the feedback divider is the reference voltage V_{REF} with 1.213 V. The typical value of the voltage at the FB pin is 0 V. The minimum recommended output voltage at the converter is –15 V. The feedback divider current should be 10 μ A. The voltage across R2 is 1.213 V. Based on those values, the recommended value for R2 should be 120 k Ω to 200 k Ω in order to set the divider current at the required value. The value of the resistor R3 can then be calculated using Equation 1, depending on the needed output voltage (V_{OUT}).

$$R3 = R2 \times \left(\frac{V_{REF} - V_{OUT}}{V_{REF}} - 1\right)$$
(1)

For example, if an output voltage of -5 V is needed and a resistor of 150 k Ω has been chosen for R2, a 619-k Ω resistor is needed to program the desired output voltage.

8.2.2.1.1 Inductor Selection

An inductive converter normally requires two main passive components for storing energy during the conversion. An inductor and a storage capacitor at the output are required.

The average inductor current depends on the output load, the input voltage V_{IN} , and the output voltage V_{OUT} . It can be estimated with Equation 2, which shows the formula for the inverting converter.

$$I_{Lavg} = \frac{V_{IN} - V_{OUT}}{V_{IN} \times 0.8} \times I_{OUT}$$

where

An important parameter for choosing the inductor is the desired current ripple in the inductor.

A ripple current value between 20% and 80% of the average inductor current can be considered as reasonable, depending on the application requirements. A smaller ripple reduces the losses in the inductor, as well as output voltage ripple and EMI. But in the same way, the inductor becomes larger and more expensive.

Keeping those parameters in mind, the possible inductor value can be calculated using Equation 3.

$$L = \frac{V_{IN} \times V_{OUT}}{\Delta I_L \times (V_{OUT} - V_{IN}) \times f}$$

where

- ΔI_L = Peak-to-peak ripple current
- f = Switching frequency

With the known inductor current ripple, the peak inductor value can be approximated with Equation 4. The peak current through the switch and the inductor depends also on the output load, the input voltage V_{IN} , and the output voltage V_{OUT} . To select the right inductor, it is recommended to keep the possible peak inductor current below the current-limit threshold of the power switch. For example, the current-limit threshold of the TPS63700 switch for the inverting converter is nominally 1000 mA.

$$I_{Lmax} = \frac{V_{IN} - V_{OUT}}{V_{IN} \times 0.8} \times I_{OUT} + \frac{\Delta I_L}{2}$$

where

• I_{LMAX} = Peak inductor current

With Equation 5, the inductor current ripple at a given inductor can be approximated.

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(5)



$$\Delta I_{L} = \frac{V_{IN} \times V_{OUT}}{L \times (V_{OUT} - V_{IN}) \times f}$$

where

- ΔI_L = Peak-to-peak ripple current
- L = Inductor value

Care has to be taken for the possibility that load transients and losses in the circuit can lead to higher currents as estimated in Equation 4. Also, the losses caused by magnetic hysteresis losses and copper losses are a major parameter for total circuit efficiency.

The following inductor series from different suppliers have been tested with the TPS63700 converter, see Table 2.

Output Voltage	Vendor	SUGGESTED INDUCTOR
–5 V	TDK	VLF4012 4.7 μH
-o v	IDK	SLF6025-4.7 μH
–5 V	Coiloroft	LPS4018 4.7 μH
-o v	Coilcraft	LPS3015 4.7 µH
-12 V	Sumida	CDRH5D18 10 µH
–12 V	Coilcraft	MOS6020 10 μH

Table 2. List of Inductors

8.2.2.2 Capacitor Selection

8.2.2.2.1 Input Capacitor

At least a 10-µF ceramic input capacitor is recommended for a good transient behavior of the regulator, and EMI behavior of the total power supply circuit.

8.2.2.2.2 Output Capacitors

One of the major parameters necessary to define the capacitance value of the output capacitor is the maximum allowed output voltage ripple of the converter. This ripple is determined by two parameters of the capacitor, the capacitance and the ESR. It is possible to calculate the minimum capacitance needed for the defined ripple, supposing that the ESR is zero, by using Equation 6 for the inverting converter output capacitor.

$$C_{min} = \frac{I_{OUT} \times V_{OUT}}{f_S \times \Delta V \times \left(V_{OUT} - V_{IN}\right)}$$

where

- f = Switching frequency
- $\Delta V = \text{Maximum allowed ripple}$

With a chosen ripple voltage in the range of 10 mV, a minimum capacitance of 12 μ F is needed. The total ripple is larger due to the ESR of the output capacitor. This additional component of the ripple can be calculated using Equation 7 .

$$\Delta V_{ESR} = I_{OUT} \times R_{ESR}$$

where

• ΔV_{ESR} = Voltage ripple caused by R_{ESR} of capacitor

(7)

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An additional ripple of 2 mV is the result of using a typical ceramic capacitor with an ESR in a 10-m Ω range. The total ripple is the sum of the ripple caused by the capacitance, and the ripple caused by the ESR of the capacitor. In this example, the total ripple is 12 mV. Additional ripple is caused by load transients. When the load current increases rapidly, the output capacitor must provide the additional current until the inductor current has been increased by the control loop by setting a higher on-time at the main switch (duty cycle). The higher duty cycle results in longer inductor charging periods, but the rate of increase of the inductor current is also limited by the inductance itself. When the load current decreases rapidly, the output capacitor needs to store the excessive energy (stored in the inductor) until the regulator has decreased the inductor current by reducing the duty cycle. The recommendation is to use higher capacitance values, as the previous calculations show.

8.2.2.3 Stabilizing the Control Loop

8.2.2.3.1 Feedback Divider

To speed up the control loop, a feed-forward capacitor of 10 pF is recommended in the feedback divider, parallel to R3.

To avoid coupling noise into the control loop from the feed-forward capacitor, the feed-forward effect can be bandwidth-limited by adding series resistor R4. A value in the range of 100 k Ω is suitable. The higher the resistance, the lower the noise coupled into the control loop system.

8.2.2.3.2 Compensation Capacitor

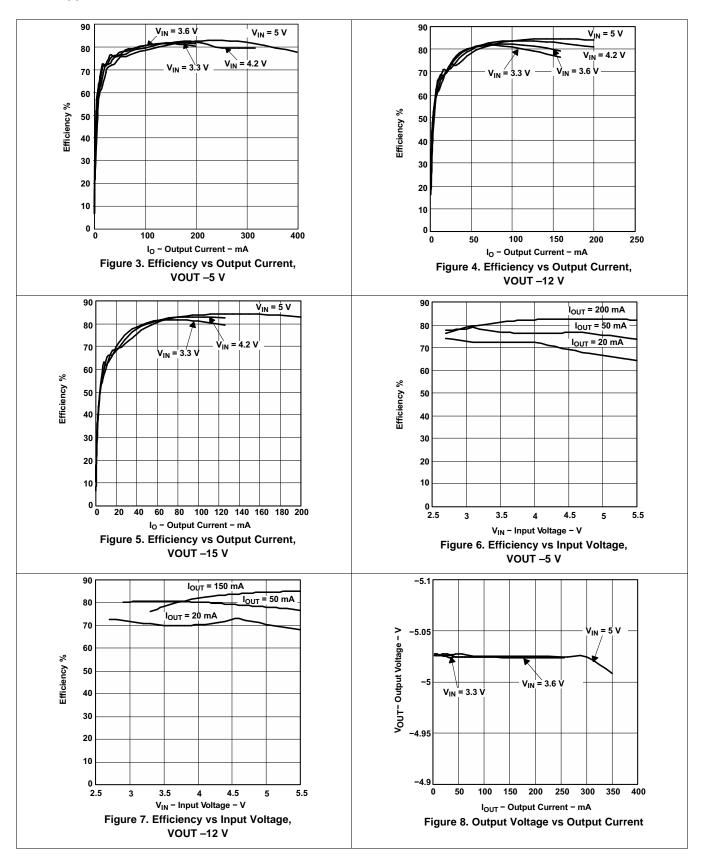
The control loop of the converter is completely compensated internally. However the internal feed-forward system requires an external capacitor. A 4.7-nF capacitor at the COMP pin of the converter is recommended.

Product Folder Links: TPS63700

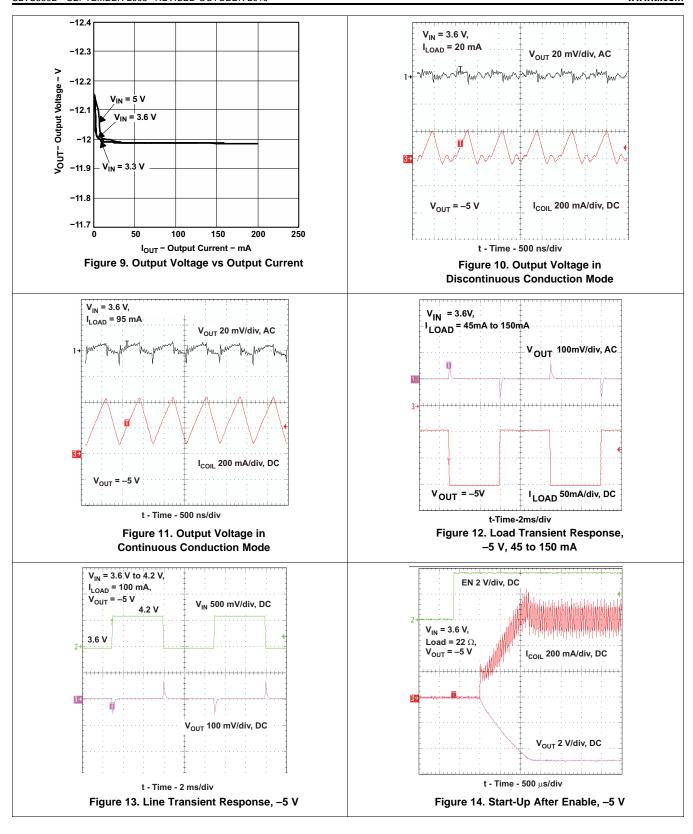
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8.2.3 Application Curves









8.3 System Example

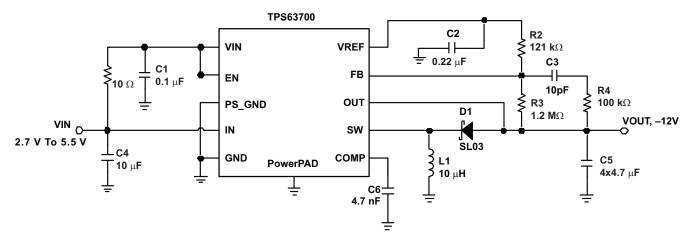


Figure 15. Circuit for -12-V Output



9 Power Supply Recommendations

The power supply to the TPS63700 needs to have a current rating according to the input supply voltage, output voltage and output current of the TPS63700.

10 Layout

10.1 Layout Guidelines

For all switching power supplies the layout is an important step in the design, especially at high peak currents and high switching frequencies. If the layout is not carefully done, the regulator could show stability problems as well as EMI problems. Therefore, use wide and short traces for the main current paths, and for the power-ground tracks. The input and output capacitors should be placed as close as possible to the IC. The diode need to be connected closest to the SW pin to minimize parasitic inductance. For low noise operation small bypass capacitors $C_{\text{IN BP}}$ and $C_{\text{OUT BP}}$ in the nF range can be added close to the IC.

The feedback divider should be placed as close as possible to the V_{REF} pin of the IC. Use short traces when laying out the control ground. Figure 18 shows the layout of the EVM board.

10.2 Layout Example

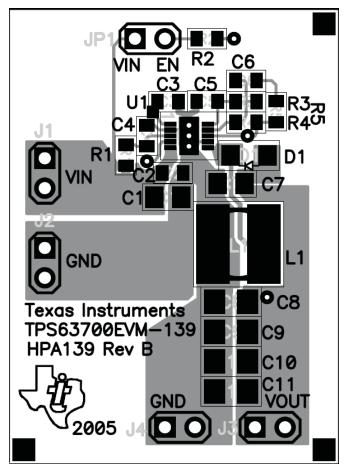


Figure 16. Layout Considerations, Top View



Layout Example (continued)

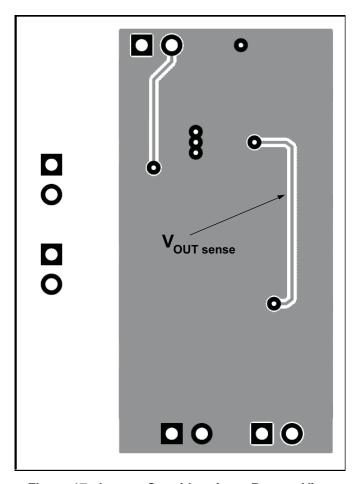


Figure 17. Layout Considerations, Bottom View

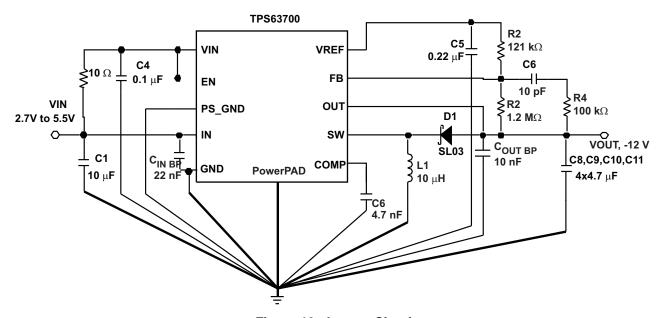


Figure 18. Layout Circuit



11 Device and Documentation Support

11.1 Device Support

11.1.1 Third-Party Products Disclaimer

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Design Support *TI's Design Support* Quickly find helpful E2E forums along with design support tools and contact information for technical support.

11.3 Trademarks

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11.4 Electrostatic Discharge Caution



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

11.5 Glossary

SLYZ022 — TI Glossary.

This glossary lists and explains terms, acronyms, and definitions.

12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

www.ti.com 2-May-2025

PACKAGING INFORMATION

Orderable part number	Status	Material type	Package Pins	Package qty Carrier	RoHS (3)	Lead finish/ Ball material	MSL rating/ Peak reflow	Op temp (°C)	Part marking (6)
						(4)	(5)		
TPS63700DRCR	Active	Production	VSON (DRC) 10	3000 LARGE T&R	Yes	NIPDAU NIPDAU	Level-2-260C-1 YEAR	-40 to 125	NUB
TPS63700DRCT	Active	Production	VSON (DRC) 10	250 SMALL T&R	Yes	NIPDAU NIPDAU	Level-2-260C-1 YEAR	-40 to 125	NUB

⁽¹⁾ Status: For more details on status, see our product life cycle.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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⁽²⁾ Material type: When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

⁽³⁾ RoHS values: Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

⁽⁴⁾ Lead finish/Ball material: Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

⁽⁵⁾ MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

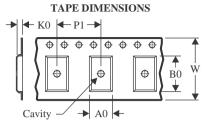
⁽⁶⁾ Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

PACKAGE MATERIALS INFORMATION

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TAPE AND REEL INFORMATION





A0	Dimension designed to accommodate the component width
В0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal

Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS63700DRCR	VSON	DRC	10	3000	330.0	12.4	3.3	3.3	1.1	8.0	12.0	Q2
TPS63700DRCT	VSON	DRC	10	250	180.0	12.5	3.3	3.3	1.1	8.0	12.0	Q2

PACKAGE MATERIALS INFORMATION

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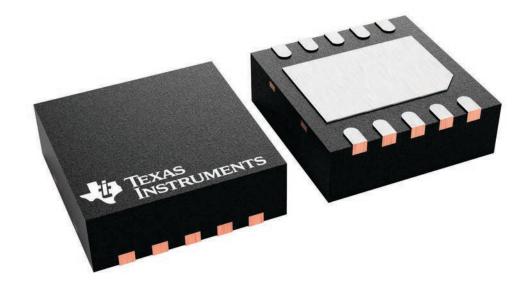
*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS63700DRCR	VSON	DRC	10	3000	356.0	356.0	35.0
TPS63700DRCT	VSON	DRC	10	250	338.0	355.0	50.0

3 x 3, 0.5 mm pitch

PLASTIC SMALL OUTLINE - NO LEAD

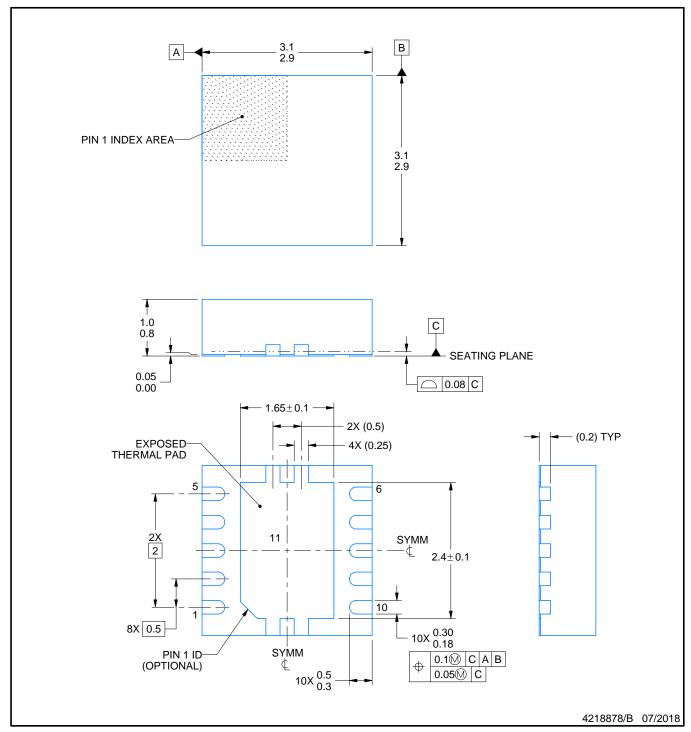
This image is a representation of the package family, actual package may vary. Refer to the product data sheet for package details.



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PLASTIC SMALL OUTLINE - NO LEAD

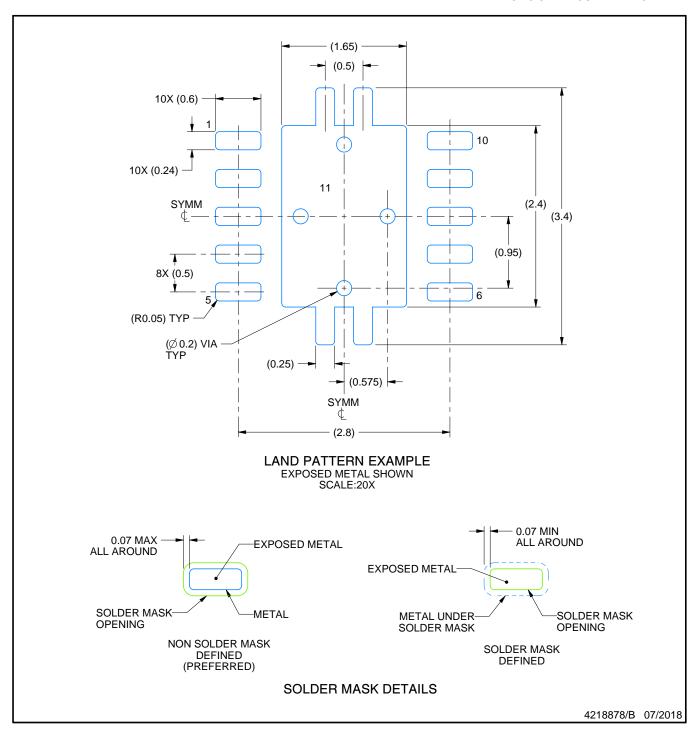


NOTES:

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
 2. This drawing is subject to change without notice.
- 3. The package thermal pad must be soldered to the printed circuit board for optimal thermal and mechanical performance.



PLASTIC SMALL OUTLINE - NO LEAD

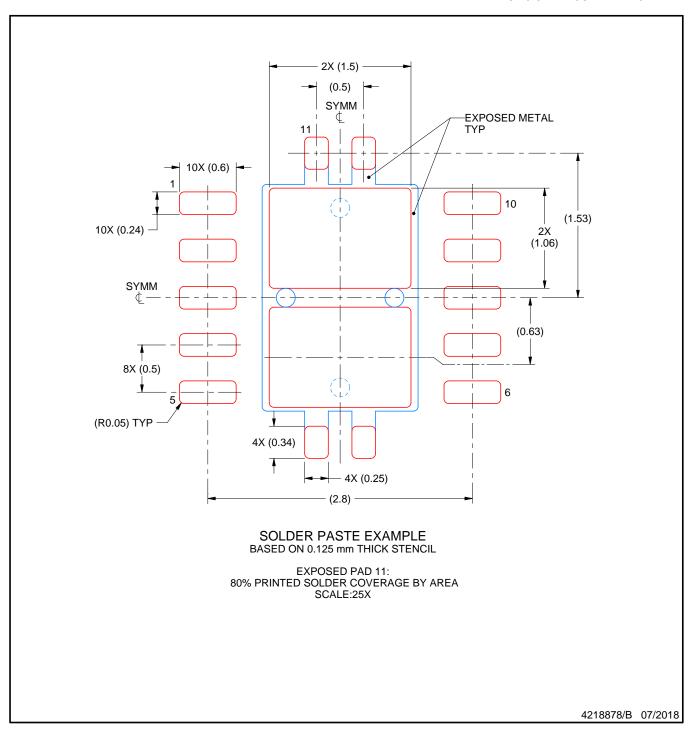


NOTES: (continued)

- 4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slua271).
- 5. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.



PLASTIC SMALL OUTLINE - NO LEAD



NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.



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